

MHD in a Cylindrical Shearing Box

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July 11th, 2019

Suzuki, Taki, & Suriano, PASJ in press (arxiv:1904.05032)

Thanks to XC40@YITP & ATERUI@CfCA/NaOJ

Global MHD Simulation of a Disk

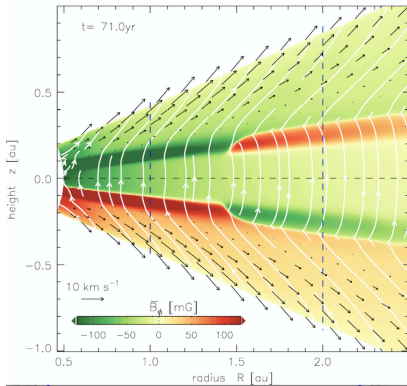
Suzuki & Inutsuka 2014

see also Hawley+ 2000; Beckwith+ 2009; Flock+ 2011; Parkin & Biknell 2013;

Takasao+ 2018; Zhu & Stone 2018 ...

Global Simulations with Non-ideal MHD

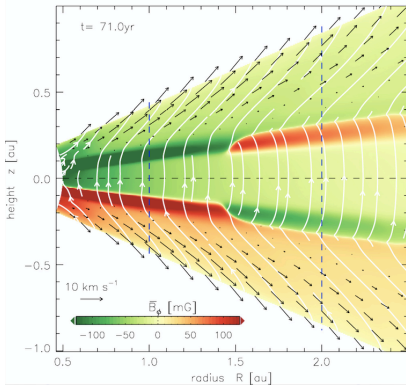
Global Simulations with Non-ideal MHD



Gressel+ 2015

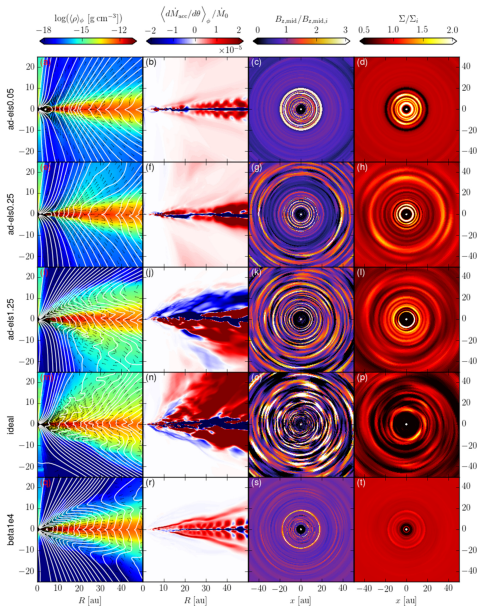
Global Simulations with Non-ideal MHD

Suriano, ... Suzuki, & Li 2019 →
see also Riols & Lesur 2018



Gressel+ 2015

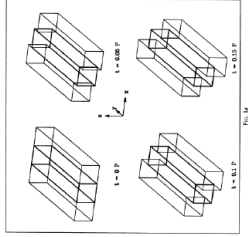
see also Flock+ 2015; Bai & Stone 2016;
Béthune, Lesur, & Ferreira 2017



Cartesian Shearing Box Simulations

Hawley et al. 1995;

Matsumoto & Tajima 1995; ...



Magnetized Disk Winds in Local Simulations

Ideal MHD (Suzuki & Inutsuka 2009) Resistive MHD (Suzuki+ 2010)

Bai & Stone 2013; Lesur+ 2014; Fromang+ 2013; Simon+ 2018; Mori+ 2018; ...

Global vs. Local

Global vs. Local

Global Simulations

Global vs.Local

Global Simulations

- Handle global effects

Global vs. Local

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- But long-time simulations not easy
 - ≈ 1000 rot. at $R_{\text{in}} \Rightarrow \lesssim 100$ rot. at R_{mid}

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- Capture fine-scale structure/turbulence

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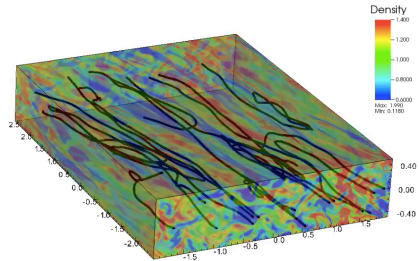
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Local Simulations

- Capture fine-scale structure/turbulence
- Perform long-time stable simulations
- But disadvantages ... \Rightarrow Next Page

Cartesian Shearing Box

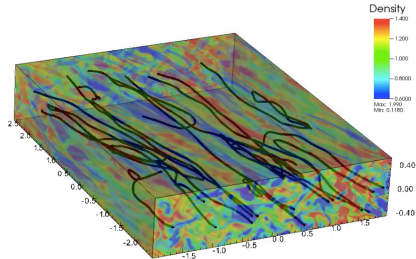
Some Disadvantages



Cartesian Shearing Box

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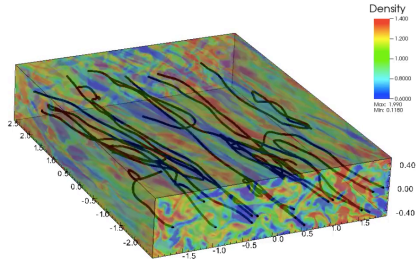
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Cartesian Shearing Box

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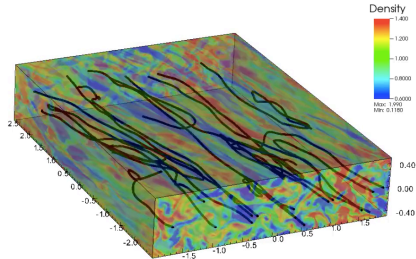
- Neglect the Curvature
 - $\pm x$ symmetry
- The central star located on either left or right



Cartesian Shearing Box

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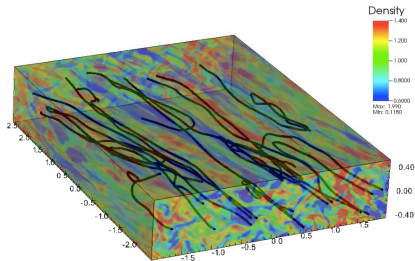
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- No Net Gas Accretion



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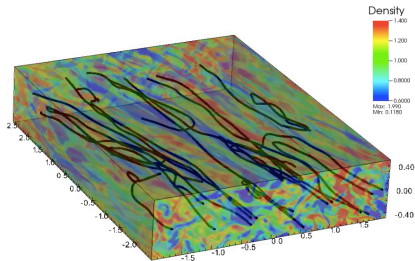
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- $\pm x$ symmetry
The central star located on either left or right
- No Net Gas Accretion
- The direction of angular momentum NOT defined
- Removal of Angular Momentum by Disk Winds NOT well-defined



Zoom-in & Zoom-out

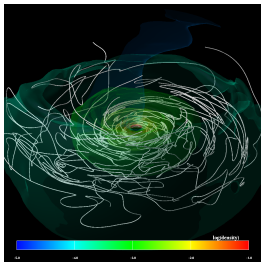
Global \leftarrow

\Rightarrow Local

Zoom-in & Zoom-out

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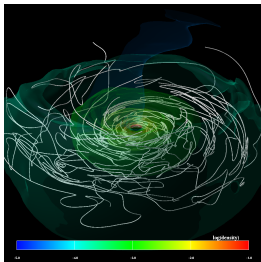


Spherical
 (r, θ, ϕ)

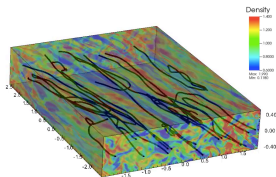
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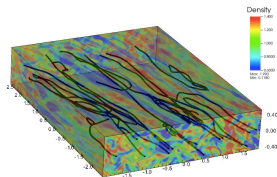
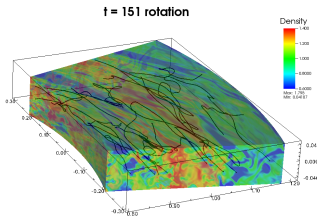
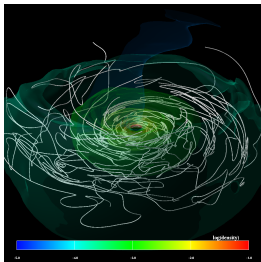


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Spherical
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Cylindrical
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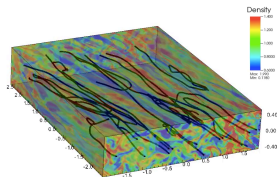
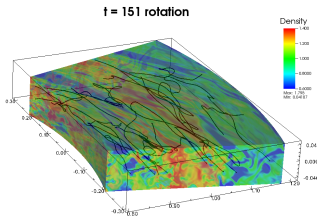
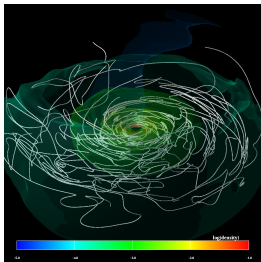
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A New Approach: “Cylindrical Shearing Box”

Zoom-in & Zoom-out

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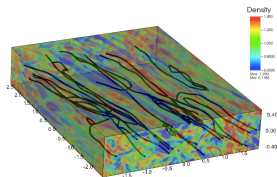
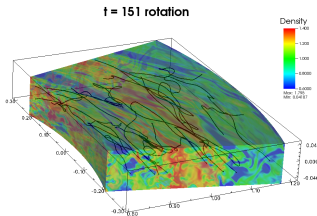
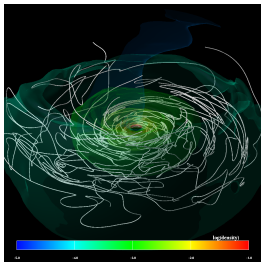
A New Approach: "Cylindrical Shearing Box"

- Break the Symmetry

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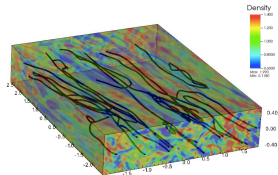
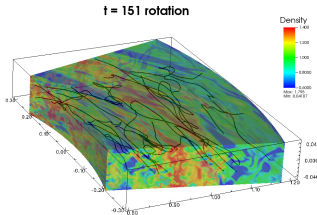
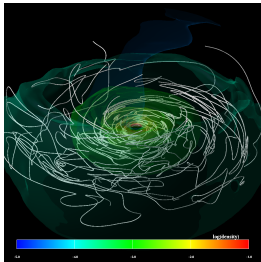
A New Approach: “Cylindrical Shearing Box”

- Break the Symmetry
- Introduce the Curvature

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A New Approach: “Cylindrical Shearing Box”

- Break the Symmetry
- Introduce the Curvature

\Rightarrow can handle the net accretion ?

Previous Attempts

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- Nonlocal Shearing Box
Add curvature terms (Brandenburg+ 1996)

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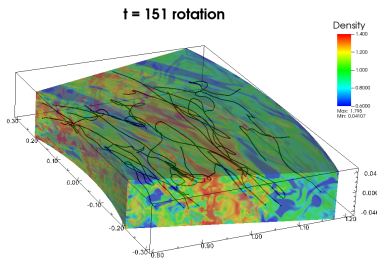
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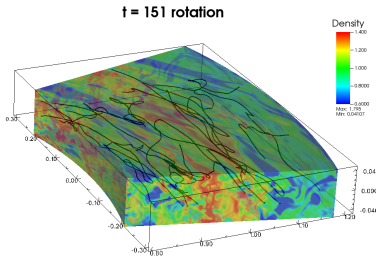
Unphysical oscillations excited
⇒ Damping zone treatment

Cylindrical Shearing Box



Cylindrical Shearing Box

Key : Boundary Condition at R_{\pm}

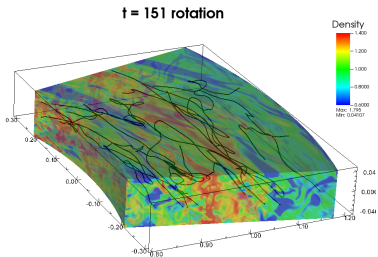


Cylindrical Shearing Box

Key : Boundary Condition at R_{\pm}

- Shear: $A(R_{\pm}, \phi, z) = A(R_{\mp}, \phi \pm \Delta\Omega_{\text{eq}}t, z)$

where $\Delta\Omega_{\text{eq}} = \Omega_{\text{eq},-} - \Omega_{\text{eq},+}$



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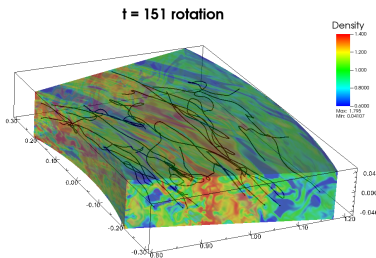
$$\text{where } \Delta\Omega_{\text{eq}} = \Omega_{\text{eq},-} - \Omega_{\text{eq},+}$$

- Radial Boundary Condition

⇐ Conservation Laws

of Mass+Momentum+(Energy)+ B

Conserved quantities, A , at R_- & R_+



$$A = \begin{cases} \rho v_R R \\ \rho v_R^2 R \\ (\rho v_R v_\phi + B_\phi B_R / 4\pi) / \Omega_{\text{eq}} \\ \rho v_R v_z R \\ v_R B_\phi - v_\phi B_R \\ (v_z B_R - v_R B_z) R \\ \text{Energy} \end{cases}$$

Shearing Radial Boundary

- Mass:

$$\partial_t \rho + R^{-1} \partial_R(\rho v_R R) + \partial_\phi(\dots) + \partial_z(\dots) = 0$$

- Momentum- R :

$$\partial_t(\rho v_R) + R^{-1} \partial_R(\rho v_R^2 R) + \dots = 0$$

- Momentum- ϕ (Angular Momentum):

$$\partial_t(\rho v_\phi R) + \partial_R[(\rho v_R v_\phi + B_R B_\phi / 4\pi) R^2] + \dots = 0$$

- Momentum- z :

$$\partial_t(\rho v_z) + R^{-1} \partial_R(\rho v_R v_z R) + \dots = 0$$

- Induction eq.- ϕ

$$\partial_t B_\phi = \partial_z(\dots) - \partial_R(v_R B_\phi - v_\phi B_R)$$

- Induction eq.- z

$$\partial_t B_z = R^{-1} \partial_R[(v_z B_R - v_R B_z) R] - \partial_\phi(\dots)$$

- Energy Equation

Simulation Details

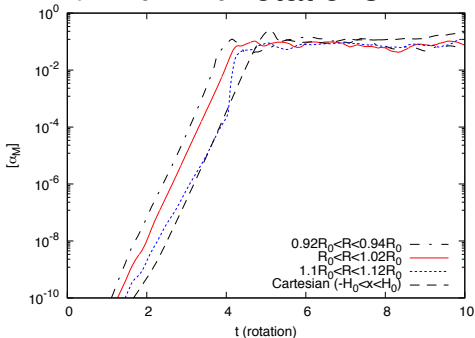
- z -Unstratified
- Ideal MHD
- $c_{s,0}/R_0\Omega_{\text{Kep},0} = H_0/R_0 = 0.1$
- local isothermal: $T = T_0 \left(\frac{R}{R_0}\right)^{-1}$
- Initial $B_z = B_{z,0} \left(\frac{R}{R_0}\right)^{-1}$; $\rho = \rho_0 \left(\frac{R}{R_0}\right)^{-1}$
with $\beta_{z,0} = 8\pi p/B_{z,0}^2 = 10^3$
- Box Size $(L_R, L_\phi, L_z) = (4H_0, (5\pi/3)H_0, H_0)$

Cylindrical Shearing Box (CySB)

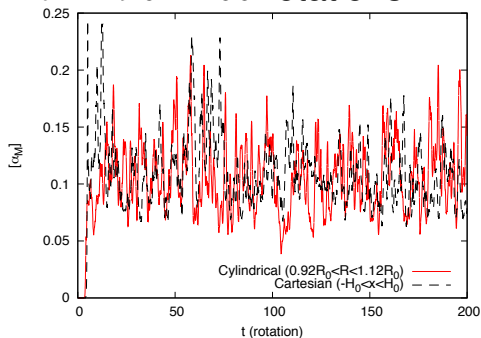
Time Evolution of α_M

$$\alpha_M = B_R B_\phi / 4\pi p$$

$t = 0 - 10$ rotations



$t = 190 - 200$ rotations

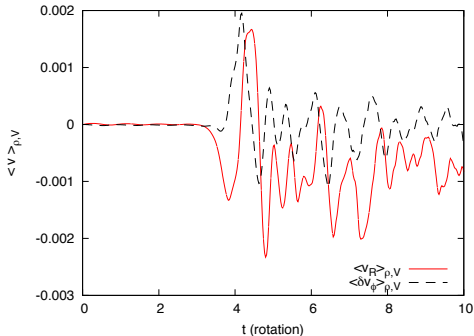


Cartesian (black dashed line)

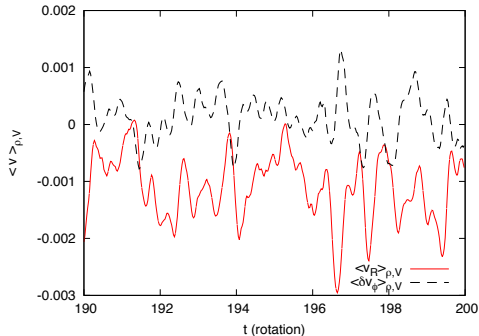
vs. Cylindrical (red solid & other lines)

Mass Accretion

$t = 0 - 10$ rotations



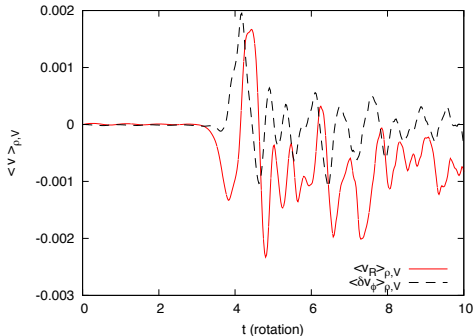
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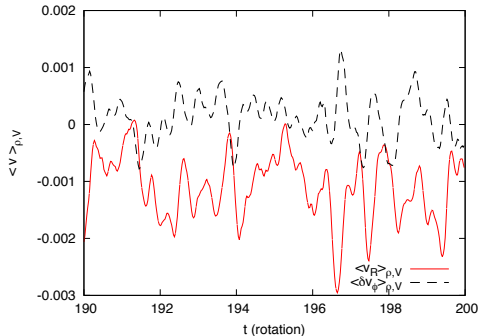
Red: v_R , Black: δv_ϕ

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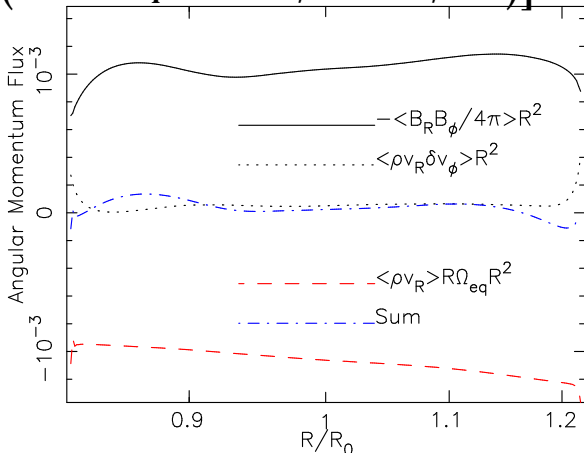
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Inward Mass Accretion is naturally induced.

Angular Momentum Flows

Under the steady-state condition:

$$\frac{\partial}{\partial R} \left[R^2 \left(\rho v_R R \Omega_{\text{eq}} + \rho v_R \delta v_\phi - B_R B_\phi / 4\pi \right) \right] = 0$$

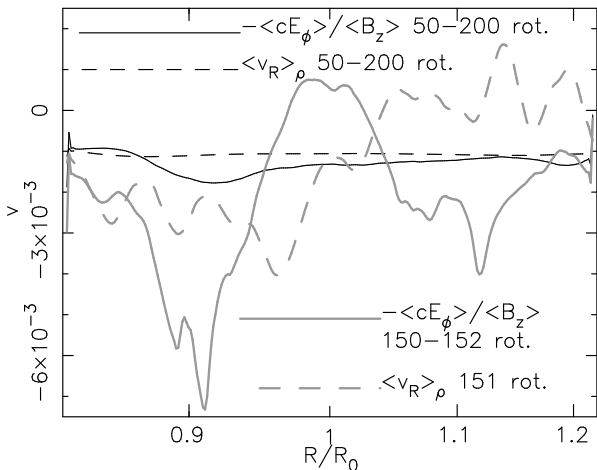


Outward A.M. flux (turbulence; black lines)
+ Inward A.M. flux (accretion; red line) ≈ 0

Accretion & B_z Advection

$$\frac{\partial}{\partial t}(RB_z) = \frac{\partial}{\partial R} [R(v_z B_R - v_R B_z)]$$

$$\Rightarrow \langle v_{R,B_z} \rangle = \langle R(v_R B_z - v_z B_R) \rangle / \langle RB_z \rangle = \langle cE_\phi \rangle / \langle B_z \rangle$$



B field and gas are slipped via turbulent diffusion

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- $\kappa_+ \neq \kappa_-$
(epicycle frequency at R_{\pm})

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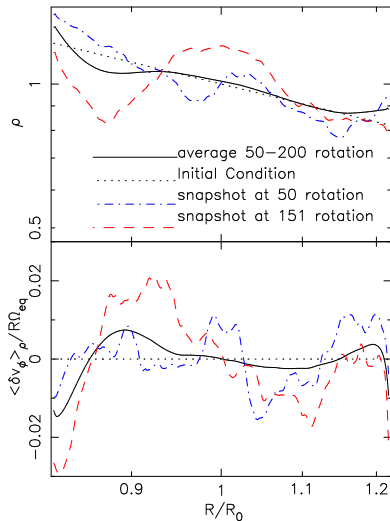
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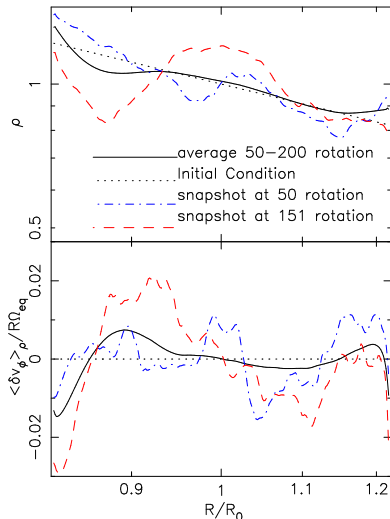
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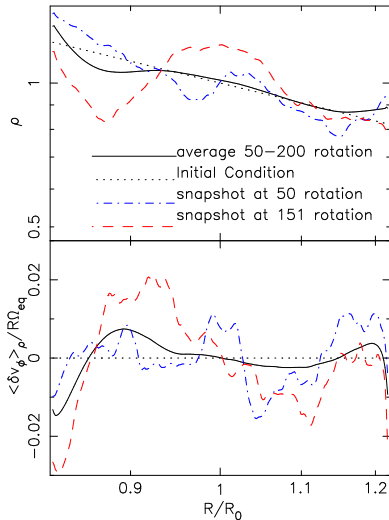
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- Extension to z -Stratified Box



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We are developing “Cylindrical Shearing Box”

–still on-going

- Handle global effects
 - net mass accretion
 - well-defined angular momentum
- Keep merits of Cartesian shearing box

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Need Your Help;
Comments & Criticism are all welcome.